



IESO_REP_0011

CONNECTION ASSESSMENT & APPROVAL PROCESS

System Impact Assessment Report

Andrews GS – Excitation System and Governor System Replacements

Applicant: Great Lakes Power - Generation

CAA ID 2004-136

Final Report

**Long Term Forecasts & Assessments Department &
Consistent Information Set Department**

December 8, 2004

System Impact Assessment Report

Andrews GS – Excitation System and Governor Replacement

1. Project Description

Great Lakes Power – Generation Division submitted a connection assessment application in which they indicate their intention to replace the generator control systems for units G1 and G2 at Andrews GS. The proposed project includes:

- Replacement of the existing excitation systems with full-static excitation systems (type IEEE ST1A); and
- Replacement of the existing governor systems with modern digital governor systems (type PTI WEHGOV).

The new excitations system will be equipped with power system stabilizers that could be connected and tuned to provide additional damping if the need is identified during commissioning tests.

2. Assessment

The IMO has assessed the impact of the proposed modifications and concluded that they are not expected to have a material impact on the reliability of the IMO-controlled grid.

This report provides the results of the impact assessment, which demonstrates that the performance of the new control systems is within the IMO market rules requirements.

Transient Stability Analysis

Based on equipment data made available by GLP, the IMO has performed dynamic simulations to verify that the transient response of the new control systems meets the market rules requirements. This modelling data is shown in Appendix A.

The results of the simulations indicate that the proposed changes for units G1 and G2 satisfy the market rules requirements. Specifically, the response ratio test and the open circuit step response test (figures 1 and 2) indicate that:

- The excitation system voltage response time is less than 50 ms (the exciter field voltage reaches 95% of the excitation ceiling voltage in less than 50 ms); and
- Following a step change in the voltage regulator reference, the proposed exciter adequately damps the field voltage and the generator terminal voltage.

The governor response test demonstrated that the governor reacted adequately to a step change in load and damped well the transient variation in turbine power. This result of this test is shown in figure 3.

The new control systems of two units at Andrews GS have also been tested for a three-phase fault on one of the Gartshore 115 kV lines between Gartshore GS and MacKay TS. The test revealed that:

- The oscillations in rotor angle, MW and MVar output, and terminal voltage at Andrews GS, Gartshore GS, MacKay GS and Hogg GS were well damped and the machines remained stable after the fault;
- The bus voltages at Third Line TS and MacKay TS recovered and were well damped after the fault;
- The MW and MVar flows on Gartshore 1 and 2, and Sault 1, 2 and 3 lines recovered and were well damped after the fault.

The plots of rotor angles, voltages, MW and MVar flows are provided in Appendix B.

3. Conclusions and IMO Requirements

The IMO's assessment concluded that the proposed project is not expected to have any adverse impact on the reliability of the IMO-controlled grid. Furthermore, the tests revealed that Andrews G1 and G2 perform adequately in dynamic conditions and there is no need to enable the power system stabiliser function of the new exciters.

4. Notification of Approval

Notification of approval is granted for the proposed upgrade project.

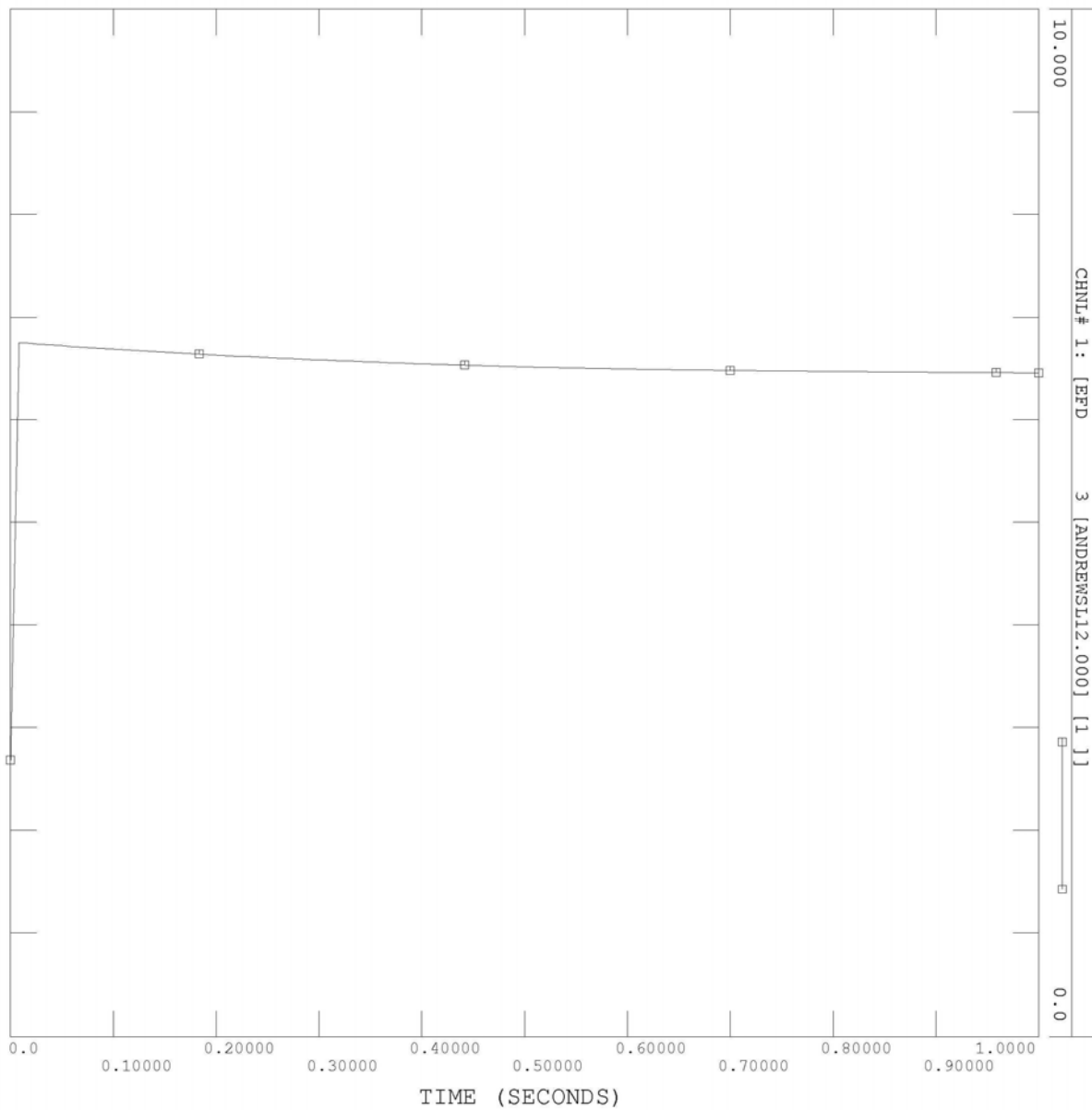


Figure 1: Exciter Response Ratio Test

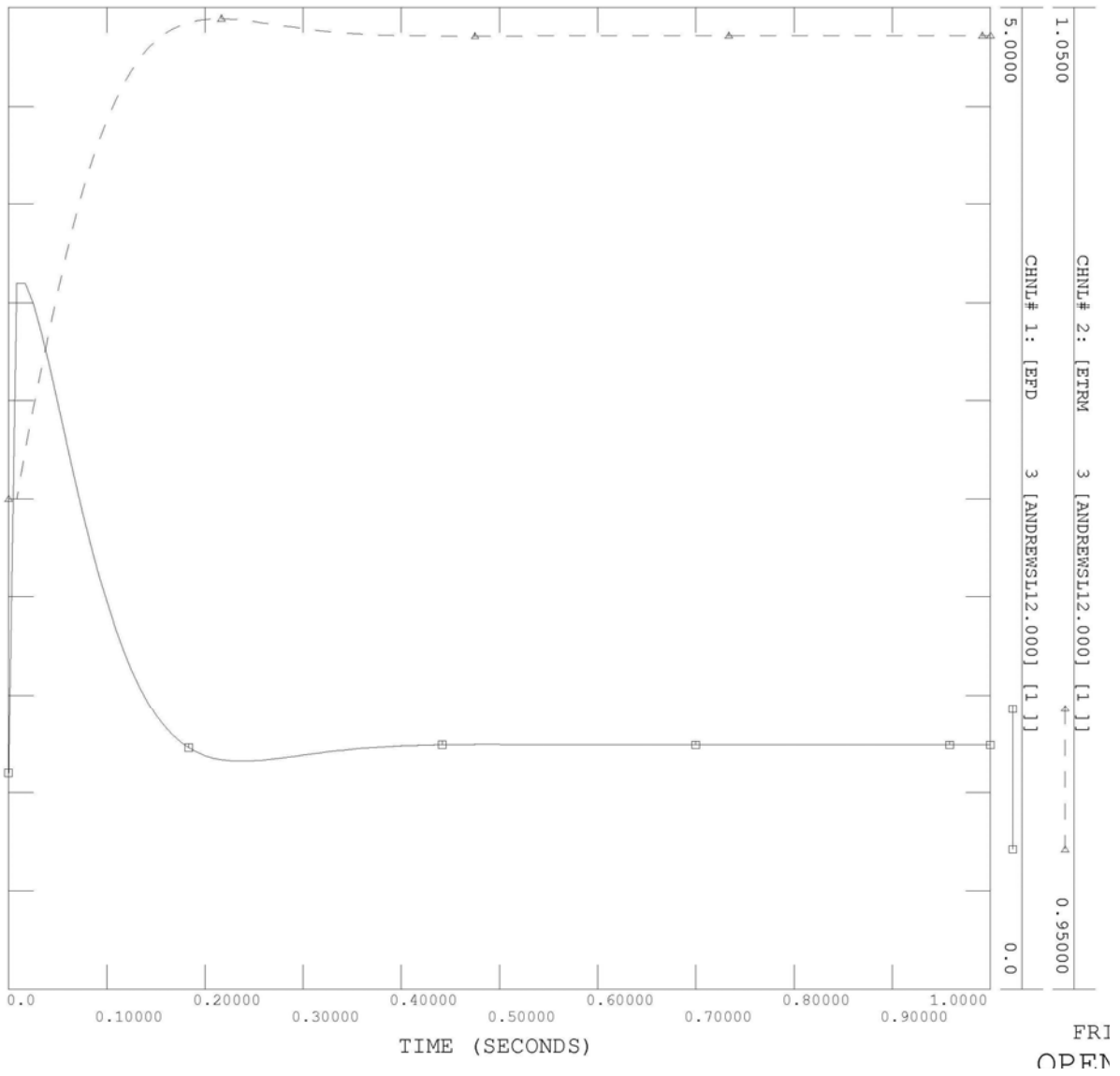


Figure 2: Exciter Open Circuit Test

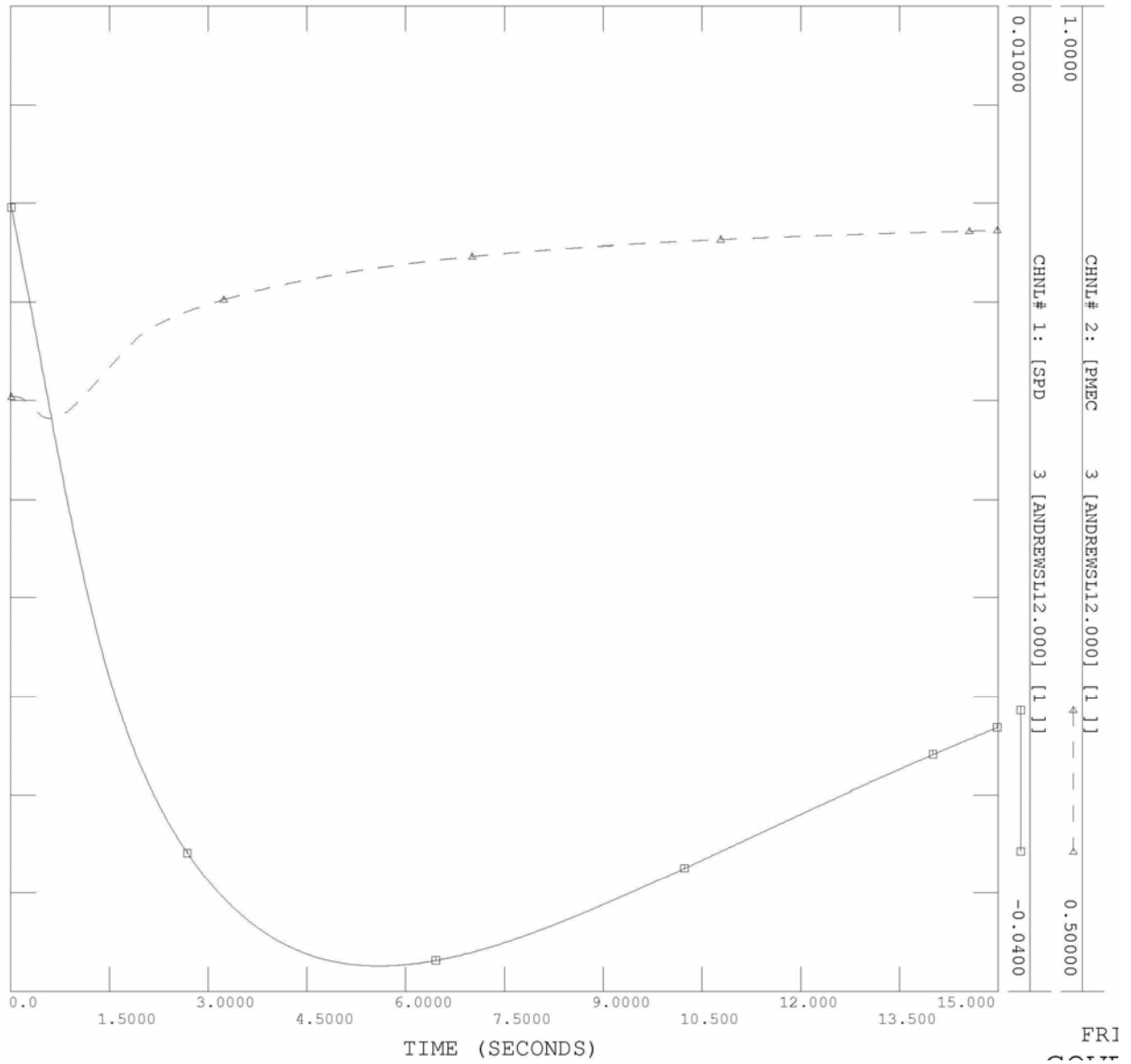


Figure 3: Governor Response Test

Appendix A

Andrews G1 modelling data

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** GENSA1 ** BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S
      10175      ANDREWG1 12.000 1  221803-221814  82204-82208

      MBASE      Z S O R C E      X T R A N      GENTAP
      11.2  0.00300+J 0.27500  0.00000+J 0.00000  1.00000

      T'D0  T''D0  T''Q0  H  DAMP  XD  XQ  X'D  X''D  XL
      3.700  0.045  0.035  2.88  0.00  1.2860  0.6400  0.3900  0.2750  0.1000

      S(1.0)  S(1.2)
      0.1000  0.6000

** ESST1A ** BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S   I C O N S
      10175      ANDREWG1 12.000 1  221833-221850  82214-82218  8749-8750

      UEL VOS      TR  VIMAX  VIMIN  TC  TB  TC1  TB1  KA
      0  0  0.015  999.000-999.000  0.000  0.000  0.000  0.000  50.0

      TA  VAMAX  VAMIN  VRMAX  VRMIN  KC  KF  TF  KLR  ILR
      0.000  999.000-999.000  6.960  -6.830  0.080  0.000  1.000  0.000  0.000

** WEHGOV ** BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S   V A R S   ICON
      10175      ANDREWG1 12.000 1  221900-221948  82226-82232  16427-16430  8752

      R-GATE  R-PE  TPE  KP  KI  KD  TD  TP  TDV  TG  GTMXOP
      0.040  0.000  1.000  2.000  0.200  0.500  0.050  0.100  0.100  0.300  0.100

      GTMXCL  GMAX  GMIN  DTURB  TW  DBAND  DPV  DICM
      -0.100  1.000  0.000  0.000  0.800  0.001  0.000  0.040

      FLOW VERSUS GATE TABLE
      G1  G2  G3  G4  G5
      0.000  1.000  0.000  0.000  0.000
      F1  F2  F3  F4  F5
      0.000  1.000  0.000  0.000  0.000

      POWER VERSUS FLOW TABLE
      F1  F2  F3  F4  F5  F6  F7  F8  F9  F10
      0.000  0.100  0.450  0.500  0.550  0.600  0.650  0.750  1.000  1.050
      P1  P2  P3  P4  P5  P6  P7  P8  P9  P10
      -0.125  0.000  0.550  0.650  0.750  0.800  0.850  0.900  1.000  1.050

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ICON(M) = 0; SIGNAL FOR DROOP IS THE GATE SIGNAL

Andrews G2 modelling data

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** GENRAL **  BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S
                10174      ANDREWG2 12.000 1  221791-221802  82199-82203

                MBASE      Z S O R C E      X T R A N      GENTAP
                11.2    0.00300+J 0.27500  0.00000+J 0.00000  1.00000

T'DO  T''DO  T''QO   H   DAMP   XD   XQ   X'D   X''D   XL
3.700  0.045  0.035  2.88  0.00  1.2860  0.6400  0.3900  0.2750  0.1000

                S(1.0)  S(1.2)
                0.1000  0.6000

** ESST1A **  BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S   I C O N S
                10174      ANDREWG2 12.000 1  221815-221832  82209-82213  8747-8748

                UEL VOS      TR      VIMAX  VIMIN      TC      TB      TC1      TB1      KA
                0   0      0.015 999.000-999.000  0.000  0.000  0.000  0.000  50.0

                TA      VAMAX  VAMIN  VRMAX  VRMIN  KC      KF      TF      KLR  ILR
                0.000 999.000-999.000  6.960 -6.830  0.080  0.000  1.000  0.000  0.000

** WEHGOV **  BUS X-- NAME --X BASEKV MC   C O N S   S T A T E S   V A R S   ICON
                10174      ANDREWG2 12.000 1  221851-221899  82219-82225  16423-16426  8751

                R-GATE  R-PE  TPE      KP      KI      KD      TD      TP      TDV      TG  GTMXOP
                0.040  0.000  1.000  2.000  0.200  0.500  0.050  0.100  0.100  0.300  0.100

                GTMXCL  GMAX  GMIN  DTURB  TW      DBAND  DPV      DICM
                -0.100  1.000  0.000  0.000  0.800  0.001  0.000  0.040

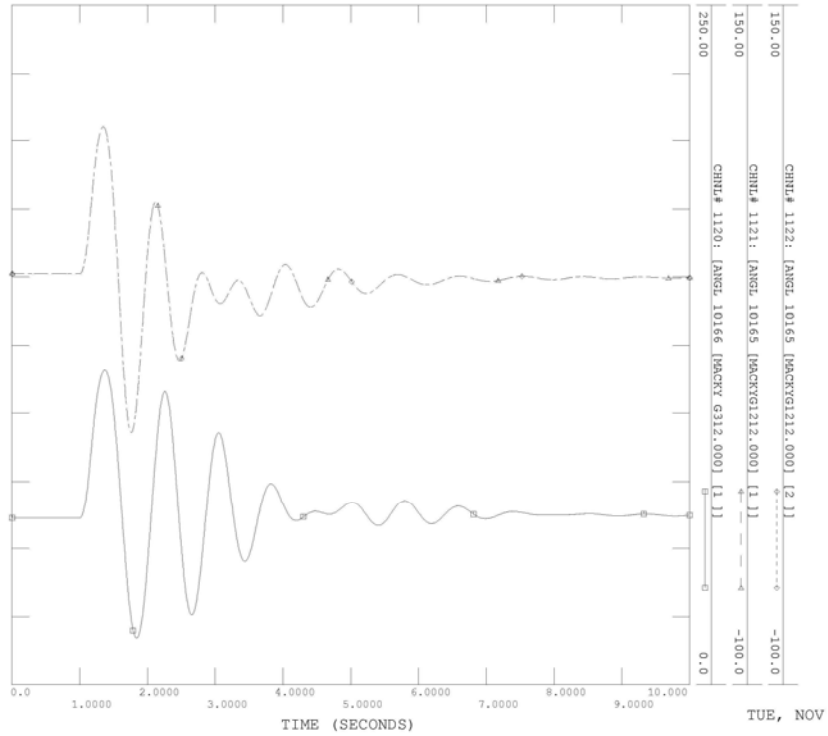
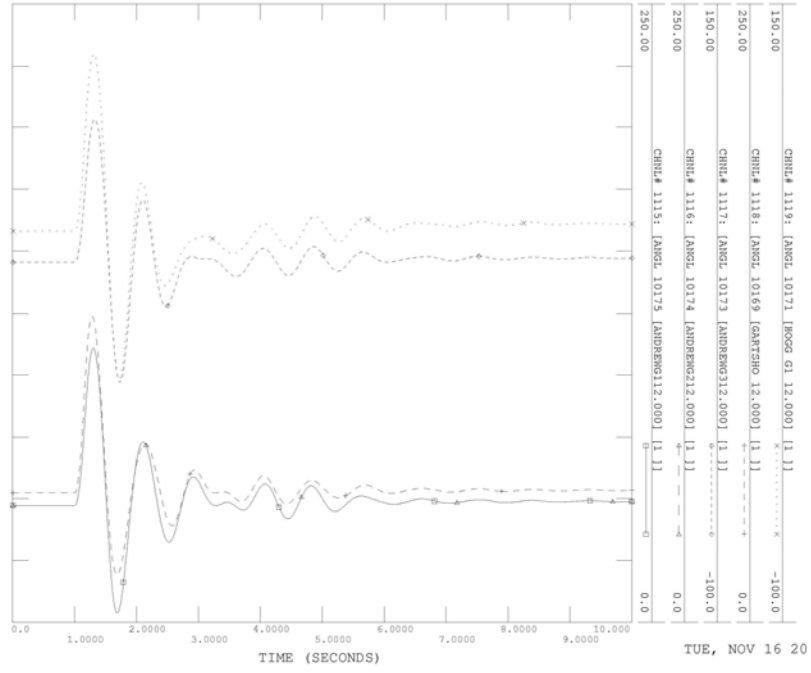
                FLOW VERSUS GATE TABLE
                G1      G2      G3      G4      G5
                0.000  1.000  0.000  0.000  0.000
                F1      F2      F3      F4      F5
                0.000  1.000  0.000  0.000  0.000

                POWER VERSUS FLOW TABLE
                F1      F2      F3      F4      F5      F6      F7      F8      F9      F10
                0.000  0.100  0.450  0.500  0.550  0.600  0.650  0.750  1.000  1.050
                P1      P2      P3      P4      P5      P6      P7      P8      P9      P10
                -0.125  0.000  0.550  0.650  0.750  0.800  0.850  0.900  1.000  1.050

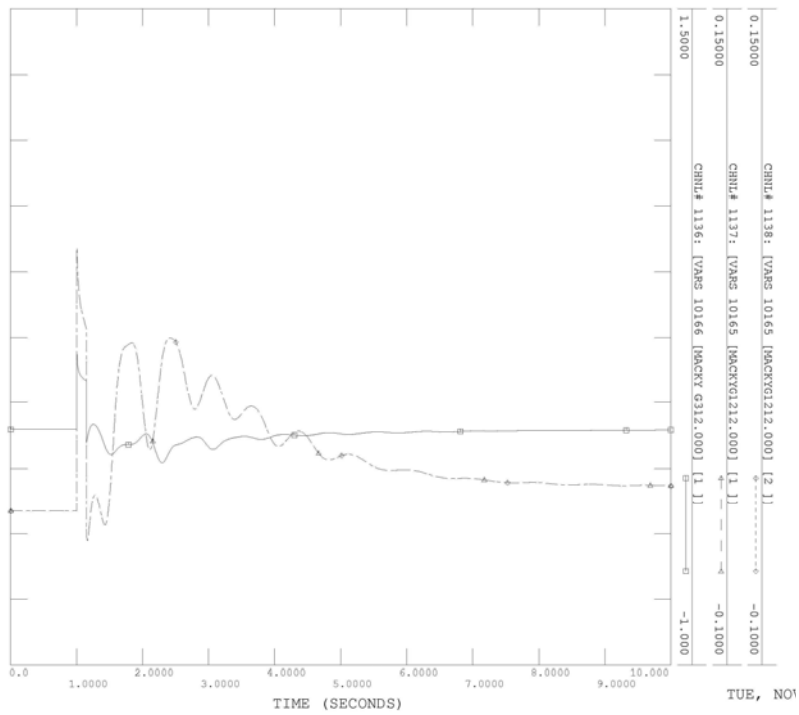
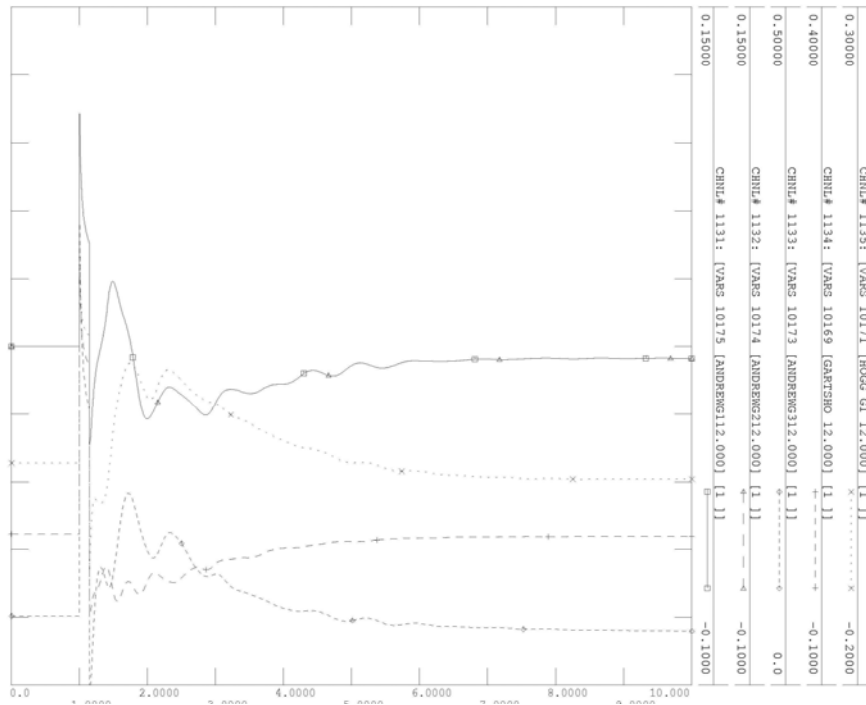
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ICON(M) = 0; SIGNAL FOR DROOP IS THE GATE SIGNAL

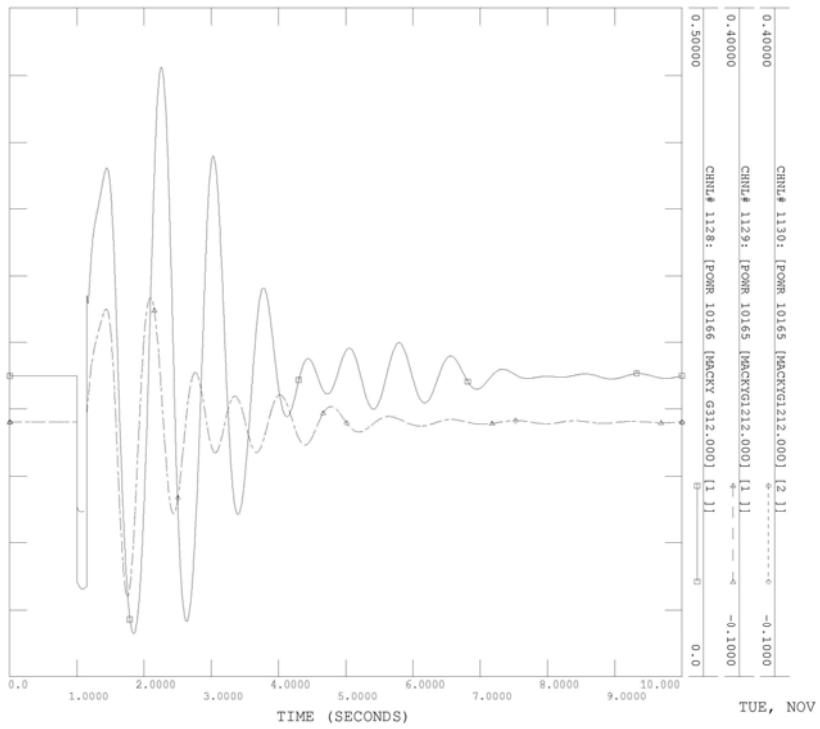
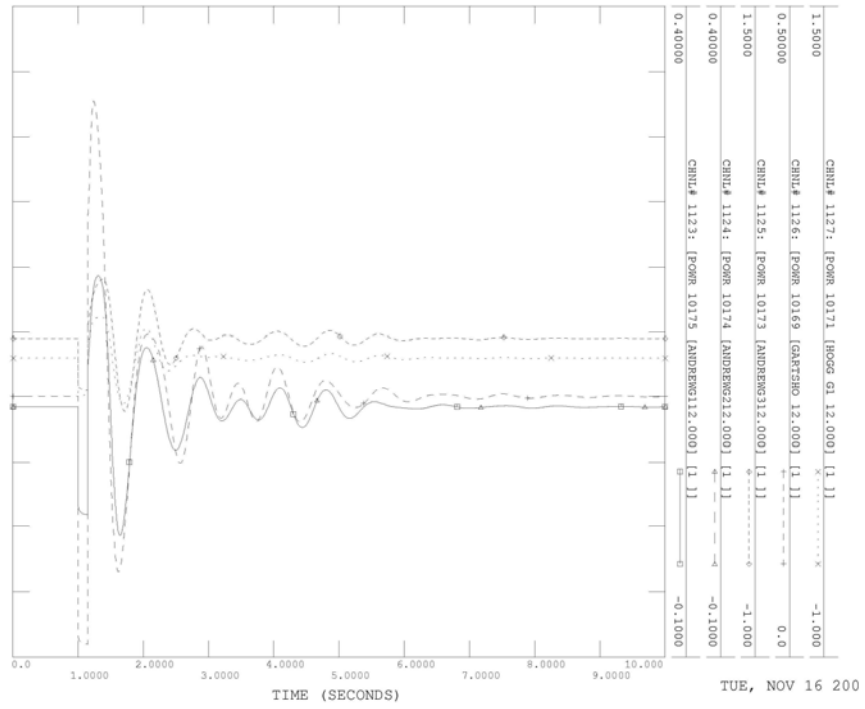
Appendix B



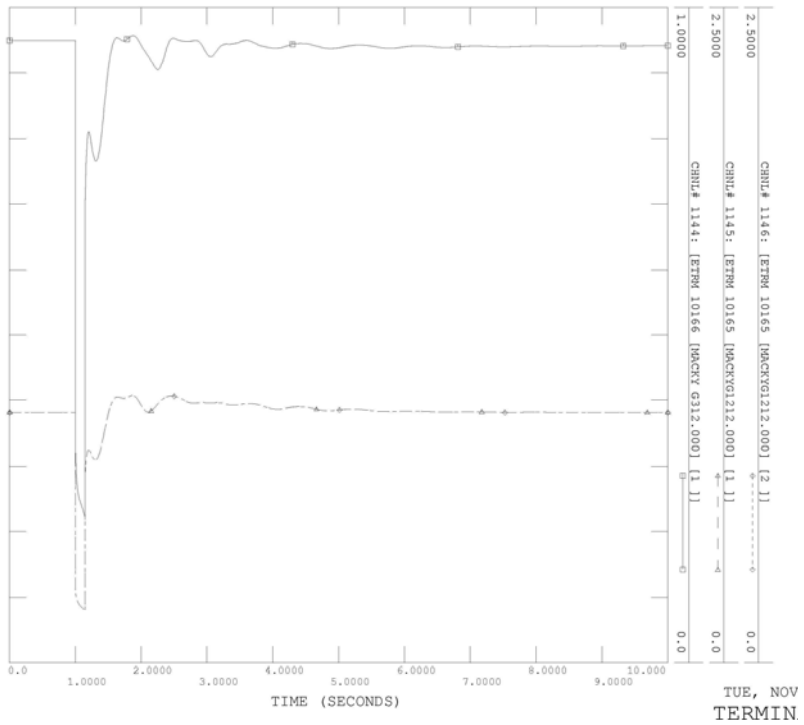
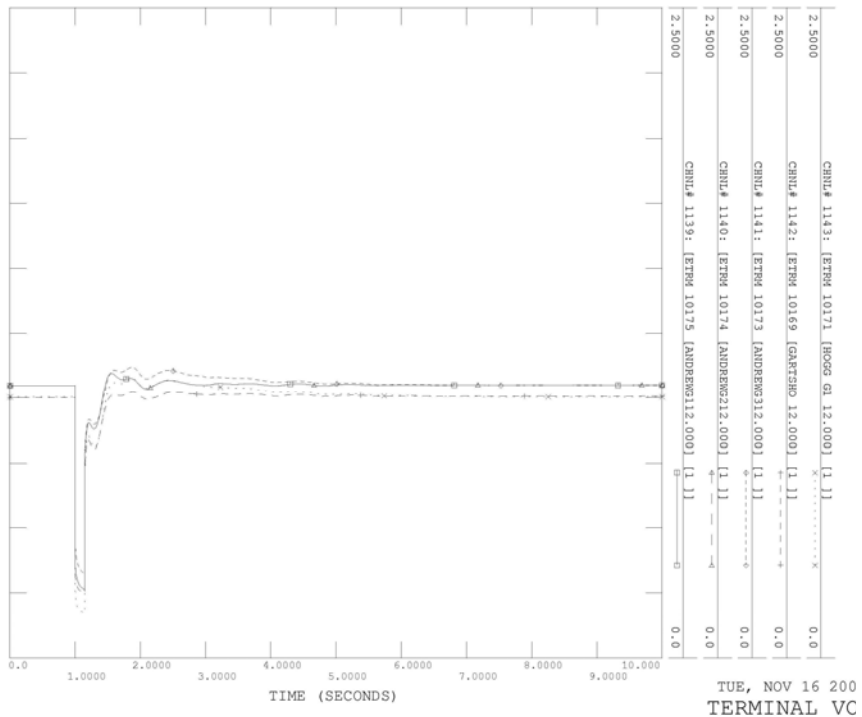
Rotor Angle Diagrams



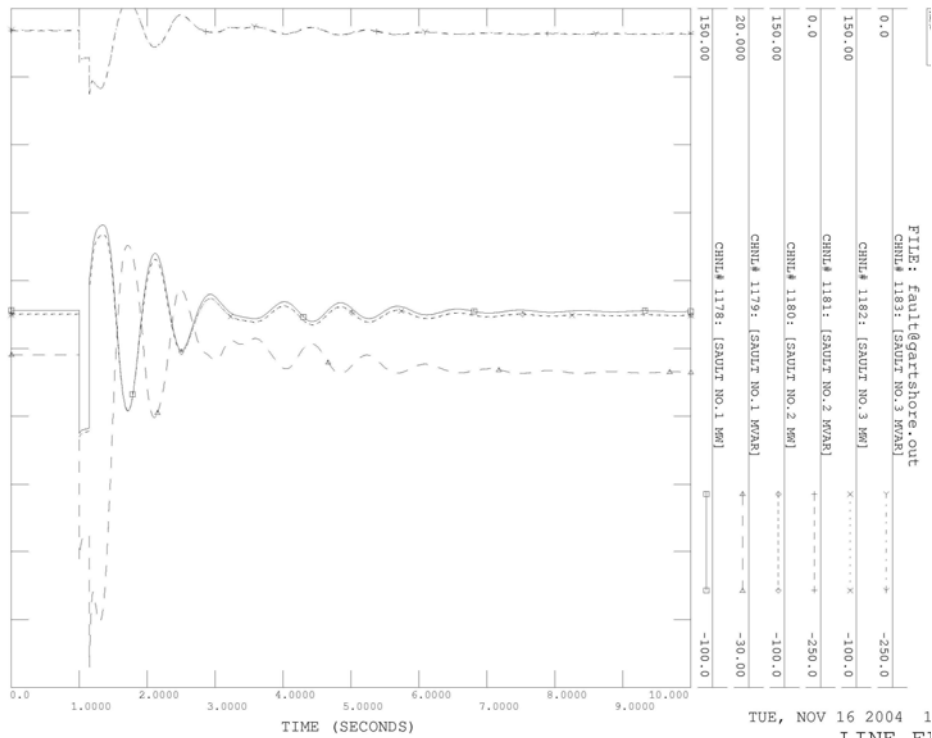
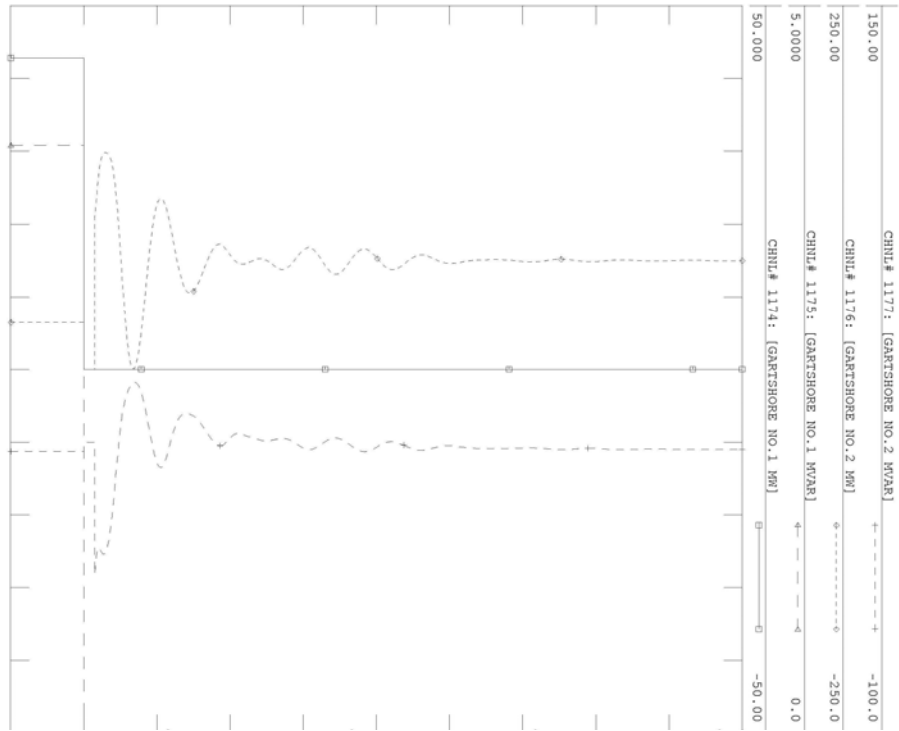
Generator MVar output diagrams



Generator MW output diagrams



Generator Terminal Voltage Diagrams



Line Flow Diagrams

